## Guidelines for Sizing

## Features

- These guidelines cover the steps which need to be taken to accurately select the correct sewage pump and applicable systems to use in sewage ejectors.

Work through the five steps below to size the system:

- System capacity (gpm required)
- Total head
- Pump selection
- Solids handling
- Basin size
- Simplex/Duplex system


## Guidelines for Sizing

## System Capacity

System Capacity refers to the rate of flow in gallons per minute (gpm) necessary to efficiently maintain the system. The "Fixture Unit" method is suggested for determining this figure. This approach assigns a relative value to each fixture or group of fixtures normally encountered. Determination of the required System Capacity is as follows:

- List all fixtures involved in the installation and using Figure 1, assign a Fixture Unit value to each. Add to obtain total.
- Referring to Figure 2, locate the total Fixture Unit amount along the horizontal axis of the graph and follow vertically until intersecting the plotted line. Read the System Capacity in gpm along the vertical axis.

Figure 1.

| FIXTURE DESCRIPTION | UNIT VALUE | TOTAL USED |
| :---: | :---: | :---: |
| Bathroom group, consisting of lavatory, bathtub or shower and (direct flush) water closet | 10 |  |
| Bathroom group, consisting of lavatory, bathtub or shower and (flush tank) water closet | 6 |  |
| Bathtub with 1-1/2" trap | 2 |  |
| Bathtub with 2" trap | 3 |  |
| Bidet with 1-1/2" trap | 3 |  |
| Dental unit or cuspidor | 1 |  |
| Drinking fountain | 1 |  |
| Dishwasher (domestic type) | 2 |  |
| Kitchen sink (domestic) | 2 |  |
| Kitchen sink (domestic with waste grinder) | 3 |  |
| Lavatory with 1-1/2" trap | 1 |  |
| Lavatory (barber or beauty shop) | 2 |  |
| Laundry tray (2-compartment) | 2 |  |
| Shower stall | 2 |  |
| Shower (group), per head | 3 |  |
| Sink (service type with floor drain) | 3 |  |
| Sink (scullery) | 4 |  |
| Sink (surgeons) | 3 |  |
| Urinal (with flush valve) | 8 |  |
| Urinal (with flush tank) | 4 |  |
| Water closet (flush valve) | 7 |  |
| Water closet (flush tank) | 3 |  |
| Swimming pools (per 1000 gal. capacity) | 1 |  |
| Unlisted fixture with 1-1/4" trap size | 2 |  |
| Unlisted fixture with 1-1/2" trap size | 3 |  |
| Unlisted fixture with 2" trap size | 4 |  |
| Unlisted fixture with 2-1/2" trap size | 5 |  |
| Unlisted fixture with 3" trap size | 6 |  |
| Unlisted fixture with 4" trap size | 7 |  |
| Water softener (domestic) | 4 |  |
| Washing machine | 2 |  |
|  | TOTAL |  |

Figure 2.


Total Head
Total Head is a combination of two components - Static Head and Friction Head - and is expressed in feet (refer to Typical Installation illustration, Figure 3).
Static Head is the actual vertical distance measured from the minimum water level in the Basin to the highest point in the discharge piping.

Friction Head is the additional head created in the discharge system due to resistance to flow within its components. All straight pipe, fittings, valves, etc. have a friction factor which must be considered. These friction factors are converted to, and expressed as, equivalent feet of straight pipe, which can then be totaled and translated to Friction Head depending on the flow and pipe size. Basically, this is reduced to four steps.

1. It will be necessary to determine the discharge pipe size. In order to ensure sufficient fluid velocity to carry solids, (generally accepted to be 2' per second), flows should be at least:

- 9 gpm through 1-1/4" pipe
- 13 gpm through 1-1/2" pipe
- 21 gpm through 2" pipe
- 30 gpm through 2-1/2" pipe
- 46 gpm through 3" pipe

2. The length of the discharge piping is measured from the discharge opening of the pump to the point of final discharge, following all contours and bends.
3. To determine the equivalent length of discharge piping represented by the various fittings and valves, refer to Figure 5 and total all values. Add this to the measured length of discharge pipe and divide by 100 to determine the number of 100' increments.
4. Refer to Figure 4 and find the required Pump Capacity (determined from Figure 2). Follow gallons per minute to pipe size being used. Multiply this number by the number of 100' increments.
Add the Static Head and Friction Head to determine Total Head.

Figure 3.


Figure 4.

| PLASTIC PIPE: FRICTION LOSS (in feet of head) PER 100 FT |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| REQ'D PUMP CAPACITY | 1-1/4" | 1-1/2" | 2" | 2-1/2" | 3" | 4" |
| GPM | ft | ft | ft | ft | ft | ft |
| 1 |  |  |  |  |  |  |
| 2 | . 10 |  |  |  |  |  |
| 3 | . 21 | . 10 |  |  |  |  |
| 4 | . 35 | . 16 |  |  |  |  |
| 5 | . 51 | . 24 |  |  |  |  |
| 6 | . 71 | . 33 | . 10 |  |  |  |
| 8 | 1.19 | . 55 | . 17 |  |  |  |
| 10 | 1.78 | . 83 | . 25 | . 11 |  |  |
| 15 | 3.75 | 1.74 | . 52 | . 22 |  |  |
| 20 | 6.39 | 2.94 | . 86 | . 36 | . 13 |  |
| 25 | 9.71 | 4.44 | 1.29 | . 54 | . 19 |  |
| 30 | 13.62 | 6.26 | 1.81 | . 75 | . 26 |  |
| 35 | 18.17 | 837 | 2.42 | 1.00 | . 35 | . 09 |
| 40 | 23.55 | 10.70 | 3.11 | 1.28 | . 44 | . 12 |
| 45 | 29.44 | 13.46 | 3.84 | 1.54 | . 55 | . 15 |
| 50 |  | 16.45 | 4.67 | 1.93 | . 66 | . 17 |
| 60 |  | 23.48 | 6.60 | 2.71 | . 93 | . 25 |
| 70 |  |  | 8.83 | 3.66 | 1.24 | . 33 |
| 80 |  |  | 11.43 | 4.67 | 1.58 | . 41 |
| 90 |  |  | 14.26 | 5.82 | 1.98 | . 52 |
| 100 |  |  |  | 7.11 | 2.42 | . 63 |
| 125 |  |  |  | 10.83 | 3.80 | . 95 |
| 150 |  |  |  |  | 5.15 | 1.33 |
| 175 |  |  |  |  | 6.90 | 1.78 |
| 200 |  |  |  |  | 8.90 | 2.27 |
| 250 |  |  |  |  |  | 3.36 |
| 300 |  |  |  |  |  | 4.85 |
| 350 |  |  |  |  |  | 6.53 |

Figure 5.

| FRICTION FACTORS FOR PIPE FITTINGS <br> IN TERMS OF EQUIVALENT FEET OF STRAIGHT PIPE |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| NOMINAL PIPE SIZE | $\begin{gathered} 90^{\circ} \\ \text { ELBOW } \end{gathered}$ | $\begin{array}{\|c\|} 45^{\circ} \\ \text { ELBOW } \end{array}$ | TEE (THROUGH FLOW) | TEE (BRANCH FLOW) | SWING CHECK VALVE | GATE <br> VALVE |
| 1-1/4 | 3.5 | 1.8 | 2.3 | 6.9 | 11.5 | 0.9 |
| 1-1/2 | 4.0 | 2.2 | 2.7 | 8.1 | 13.4 | 1.1 |
| 2 | 5.2 | 2.8 | 3.5 | 10.3 | 17.2 | 1.4 |
| 2-1/2 | 6.2 | 3.3 | 4.1 | 12.3 | 20.3 | 1.7 |
| 3 | 7.7 | 4.1 | 5.1 | 15.3 | 25.5 | 2.0 |


| TOTAL HEAD REQUIRED |  |  |
| :---: | :---: | :---: |
| (A) STATIC HEAD |  |  |
| (B) TOTAL LENGTH OF PIPING |  |  |
| (C) TOTAL FRICTION FACTORS OF FITTINGS |  |  |
| (D) TOTAL (B+C) |  |  |
| (E) DIVIDED (D) BY 100 |  |  |
| (F) HEAD LOSS PER 100 FT. OF PIPE (from Figure 4) |  |  |
| (G) FRICTION HEAD (ExF) |  |  |
| (H) TOTAL HEAD (A+G) |  |  |

## Pump Selection

Every centrifugal pump has a unique performance curve. This curve illustrates the relationship of flow (gpm) to pressure (Total Head) at any point. The pump will operate at any point along this performance curve.
Pump capacity is therefore the flow the pump will generate at any specific pressure. The object is to select a pump whose performance curve passes either through or close to the design condition, preferably above. Refer to Figure 7.

## Solids Handling

Solids Handling requirements may be determined by local codes and/or by the type of application and types of solids anticipated. Unless otherwise stated by codes, a sewage pump should have the capability of handling spherical solids of at least 2" in diameter in installations involving a water closet.

## Basin Size

Basin selection is best accomplished by relating to required System Capacity as determined by the Fixture Unit method.
Figure 6 shows recommended basin diameters, assuming the normal pump differential (distance in inches between turn-on and turn-off), and running time ranges from 15 seconds to 4 minutes. Basin depth, however, should be at least 24 " below basin inlet for most pumps and deeper where greater pumping differentials are anticipated.
NOTE: Since basin size is directly related to frequency of pump operation, it is important to select a basin of sufficient size to ensure that the pump does not short cycle.

The question of whether to use a Simplex or Duplex system depends on the type of installation and/or local codes. Generally, a determination can be made using the following guidelines.

1. Domestic: Simplex System is usually adequate.
2. Commercial: Optional - Depending on the type of business and the need for uninterrupted sanitary drainage facilities.
3. Public or Industrial: Duplex System is essential.

While you are sizing the system and before you select the pump, you will need to know and consider or make allowances for the following:

- Volts/Phase/Hertz - What is available?
- Will the pump share a circuit?
- Does the home, business, etc. have circuit breakers or fuses?
- What is the breaker or fuse Amp rating? Make sure it is enough.
- Check local or state codes for:
- Solid size requirements
- Amp ratings/circuit cord size/ratings or type
- Pipe material/size/depth to bury
- Tank size/location
- Are there plans for future expansion? As in, adding upstairs bath, basement plumbing, washing machine, etc.

Figure 6.
BASIN SIZING

|  |  | BASIN DIAMETER (inches) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 18" | 24" | 30" | 36" | 42" | 48" |
|  | 20 |  |  |  |  |  |  |
|  | 25 |  |  |  |  |  |  |
|  | 30 |  |  |  |  |  |  |
|  | 35 |  |  |  |  |  |  |
|  | 40 |  |  |  |  |  |  |
|  | 45 |  |  |  |  |  |  |
|  | 50 |  |  |  |  |  |  |
|  | 60 |  |  |  |  |  |  |
|  | 70 |  |  |  |  |  |  |
|  | 80 |  |  |  |  |  |  |
|  | 90 |  |  |  |  |  |  |
|  | 100 |  |  |  |  |  |  |
|  | 125 |  |  |  |  |  |  |
|  | 150 |  |  |  |  |  |  |
|  | 175 |  |  |  |  |  |  |
|  | 200 |  |  |  |  |  |  |
|  | 225 |  |  |  |  |  |  |
| GALLO OF BAS | $\begin{aligned} & \text { FOOT } \\ & \text { DEPTH } \end{aligned}$ | 13.2 | 23.9 | 36.7 | 52.9 | 72.0 | 94.0 |
| GALLO OF BA | $\begin{aligned} & \text { N 2-1/2' } \\ & \hline \text { FFPTH } \end{aligned}$ | 33.0 | 59.7 | 91.7 | 132.2 | 180.0 | 235.0 |

Select minimum basin depth so that 2-1/2' of basin depth in gallons = Pump capacity in gpm = Acceptable basin size

## Example Sizing Problem

What Pump Capacity would be required to handle the drainage from a 4 bathroom home, also including a dishwasher, a washer, a laundry tray, a kitchen sink, water softener, basement shower, a 13,000 gallon pool, and a bar sink (1-1/2" trap)?

1. From Figure 1:

| DESCRIPTION | FIXTURE <br> UNITS |
| :--- | :---: |
| Four bathroom groups | 24 |
| Water softener | 4 |
| Dishwasher | 2 |
| Washing machine | 2 |
| Laundry tray | 2 |
| Kitchen sink with disposal | 3 |
| Basement shower | 2 |
| Swimming pool | 13 |
| Bar sink (unlisted 1-1/2") | 3 |
| FIXTURE UNITS TOTAL | $\mathbf{5 5}$ |

2. Refer to Figure 2:

Find 55 Fixture Units on the horizontal axis. Follow vertically until intersecting the line then horizontally to the left. The
Pump Capacity on the vertical axis is 30 gpm .
Determine the Total Head of the installation illustrated in Figure 3, the Typical Installation Illustration:

1. That Static Head in this instance is $7^{\prime}$.
2. Friction Head:
a. Since the required Pump Capacity in this illustration of 30 gpm is less than the 46 gpm necessary to carry solids through $3^{\prime \prime}$ pipe, $2^{\prime \prime}$ or 2-1/2" pipe should be used. If 3" pipe is preferred or required, a Pump Capacity of at least 46 gpm is required.
b. Measurement of the length of the discharge pipe totals 200'.
c. Refer to Figure 6 and note the friction factor in equivalent feet for each fitting:

| $3-90^{\circ}$ elbows, 2" | 16 - equivalent feet |
| :---: | :--- |
| $1-$ gate valve, 2" | 1 -equivalent foot |
| 1 - swing check valve, 2" | 17 - equivalent feet |
| Total: | 34 - equivalent feet |

Adding 34 ' to the measured pipe length, the total effective pipe length becomes 234 ' or 2.34100 ' increments.
d. Refer to Figure 4, find the 30 gpm required Pump Capacity on the left scale and follow over to the 2" PVC pipe size column. Friction Head is $1.8 \times 2.34=4.2^{\prime}$.
3. Total Head Required:

Total Head $=$ Static Head + Friction Head
Example:

$$
\begin{aligned}
& \text { Total Head }=7+4.2 \\
& \text { Total Head }=11.2
\end{aligned}
$$

Due to the existence of water closets in this installation, a pump with 2" Solids Handling capacity should be used unless otherwise specifically stated by applicable codes. Use Figure 7 to select pump.

To determine the Basin size, find the Pump Capacity ( 30 gpm ) in the column on the left of Figure 6. Any Basin diameter of 18" or greater is acceptable.

Since this application is domestic, a Simplex System is sufficient.

Summary: Recommended selections for this installation would be a Simplex System utilizing an 18" or greater diameter Basin and a 2" Solids Handling pump capable of delivering at least 30 gpm at 11' $^{\prime}$.

## Summary Worksheet

## Number of Fixture Units

Flow Rate - Gallons Per Minute
Total Head Required
Pump Selection

## Typical Single Family Dwelling Sewage Pump Chart

Note: The data contained herein is for reference only. Proper sizing and selection of sewage pumps requires consideration of many factors. Always consult applicable local codes before installing any equipment. This chart is based on a residential application with not more than 34 fixture units (values assigned to each plumbing fixture). The TDH (Total Dynamic Head) of the system is calculated based on total vertical lift, horizontal length of discharge piping, and the friction losses for $2^{\prime \prime}$ diameter plastic pipe ( $3^{\prime \prime}$ diameter plastic pipe where the 16 S pump is shown).

## Total Length of Discharge Pipe in Feet

|  | 100' | 150' | 200' | 250' | 300' | 350' | 400' | 450' | 500' | 550' | 600' | 650' | 700' | 750' | 800' |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| VERT. <br> LIFT | TDH PUMP GPM | TDH PUMP GPM | TDH PUMP GPM | TDH PUMP GPM | TDH PUMP GPM | TDH PUMP GPM | TDH PUMP GPM | TDH PUMP GPM | TDH PUMP GPM | TDH PUMP GPM | TDH PUMP GPM | TDH PUMP GPM | TDH PUMP GPM | TDH PUMP GPM | TDH PUMP GPM |
| 5' | $\begin{gathered} 6.3^{\prime} \\ 9 \mathrm{SN} \\ 97 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 7.0^{\prime} \\ 9 \mathrm{SN} \\ 95 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 7.5^{\prime} \\ 9 \mathrm{SN} \\ 92 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 8.3^{\prime} \\ 9 \mathrm{SN} \\ 88 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 8.9 ' \\ 9 \mathrm{SN} \\ 82 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 9.6 ' \\ 9 \mathrm{SN} \\ 77 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 10.2^{\prime} \\ 9 \mathrm{SN} \\ 72 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 10.9^{\prime} \\ 9 \mathrm{SN} \\ 67 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 11.5^{\prime} \\ 9 \mathrm{SN} \\ 61 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 12.2^{\prime} \\ 9 \mathrm{SN} \\ 54 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 12.8^{\prime} \\ 9 \mathrm{SN} \\ 48 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 13.5^{\prime} \\ 9 \mathrm{SN} \\ 43 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 14.1^{1} \\ 9 \mathrm{SN} \\ 38 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 14.8^{\prime} \\ 9 \mathrm{SN} \\ 32 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 15.4^{\prime} \\ 9 \mathrm{SN} \\ 27 \mathrm{gpm} \end{gathered}$ |
| 6 | $\begin{gathered} 7.3^{\prime} \\ 9 \mathrm{SN} \\ 93 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 8.0^{\prime} \\ 9 \mathrm{SN} \\ 89 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 8.6^{\prime} \\ 9 \mathrm{SN} \\ 83 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 9.3^{\prime} \\ 9 \mathrm{SN} \\ 78 \mathrm{gpm} \\ \hline \end{gathered}$ | $\begin{gathered} 9.9{ }^{\prime} \\ 9 \mathrm{SN} \\ 75 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 10.6^{\prime} \\ 9 \mathrm{SN} \\ 69 \mathrm{gpm} \end{gathered}$ | $\begin{aligned} & 11.2^{\prime} \\ & 9 \mathrm{SN} \end{aligned}$ $63 \mathrm{gpm}$ | $\begin{gathered} 11.9^{\prime} \\ 9 \mathrm{SN} \\ 57 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 12.5^{\prime} \\ 9 \mathrm{SN} \\ 52 \mathrm{gpm} \\ \hline \end{gathered}$ | $\begin{gathered} 13.5^{\prime} \\ 9 \mathrm{SN} \\ 43 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 13.8^{\prime} \\ 9 \mathrm{SN} \\ 40 \mathrm{gpm} \\ \hline \end{gathered}$ | $\begin{array}{r} 14.5^{\prime} \\ 9 \mathrm{SN} \\ 33 \mathrm{gpm} \end{array}$ | $\begin{gathered} 15.1^{1} \\ 9 \mathrm{SN} \\ 29 \mathrm{gpm} \end{gathered}$ | $\begin{array}{r} 15.8^{\prime} \\ 9 \mathrm{SN} \\ 25 \mathrm{gpm} \\ \hline \end{array}$ | $\begin{gathered} 16.4^{\prime} \\ 10 \mathrm{SN} \\ 57 \mathrm{gpm} \end{gathered}$ |
| $7{ }^{\prime}$ | 8.3' 9SN <br> 88 gpm | $\begin{gathered} 9.0^{\prime} \\ 9 \mathrm{SN} \\ 81 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 9.6^{\prime} \\ 9 \mathrm{SN} \\ 77 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 10.3^{\prime} \\ 9 \mathrm{SN} \\ 70 \mathrm{gpm} \end{gathered}$ | $10.9$ $9 \mathrm{SN}$ <br> 67 gpm | $\begin{gathered} 11.6^{\prime} \\ 9 \mathrm{SN} \\ 59 \mathrm{gpm} \end{gathered}$ | $\begin{array}{r} 12.2^{\prime} \\ 9 \mathrm{SN} \\ 54 \mathrm{gpm} \end{array}$ | $\begin{gathered} 12.9^{\prime} \\ 9 \mathrm{SN} \\ 47 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 13.5^{\prime} \\ 9 \mathrm{SN} \\ 43 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 14.2^{\prime} \\ 9 \mathrm{SN} \\ 36 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 14.8^{\prime} \\ 9 \mathrm{SN} \\ 32 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 15.5^{\prime} \\ 9 \mathrm{SN} \\ 26 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 16.1^{\prime} \\ 10 \mathrm{SN} \\ 62 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 16.8^{\prime} \\ 10 \mathrm{SN} \\ 54 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 17.4^{\prime} \\ 10 \mathrm{SN} \\ 48 \mathrm{gpm} \end{gathered}$ |
| 8' | $\begin{gathered} 9.3^{\prime} \\ 9 \mathrm{SN} \\ 78 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 10.0 \\ 9 \mathrm{SN} \\ 76 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 10.6^{\prime} \\ 9 \mathrm{SN} \\ 69 \mathrm{gpm} \\ \hline \end{gathered}$ | $\begin{gathered} 11.3^{\prime} \\ 9 \mathrm{SN} \\ 62 \mathrm{gpm} \end{gathered}$ | $11.9^{\prime}$ 9SN 57 gpm | $\begin{gathered} 12.6^{\prime} \\ 9 \mathrm{SN} \\ 50 \mathrm{gpm} \end{gathered}$ | 13.2' 9SN 45 gpm | $\begin{gathered} 13.9 ' \\ 9 \mathrm{SN} \\ 39 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 14.5^{\prime} \\ 9 \mathrm{SN} \\ 33 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 15.2^{\prime} \\ 9 \mathrm{SN} \\ 28 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 15.8^{\prime} \\ 9 \mathrm{SN} \\ 25 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 16.5^{\prime} \\ 10 \mathrm{SN} \\ 56 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 17.1^{\prime} \\ 10 \mathrm{SN} \\ 52 \mathrm{gpm} \\ \hline \end{gathered}$ | $\begin{gathered} 17.8^{\prime} \\ 10 \mathrm{SN} \\ 46 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 18.4^{\prime} \\ 10 \mathrm{SN} \\ 41 \mathrm{gpm} \\ \hline \end{gathered}$ |
| $9 '$ | $\begin{gathered} 10.3^{\prime} \\ 9 \mathrm{SN} \\ 70 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 11.0^{\prime} \\ 9 \mathrm{SN} \\ 65 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 11.6^{\prime} \\ 9 \mathrm{SN} \\ 59 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 12.3^{\prime} \\ 9 \mathrm{SN} \\ 53 \mathrm{gpm} \end{gathered}$ | $12.9^{\prime}$ 9SN 47 gpm | $\begin{gathered} 13.4^{\prime} \\ 9 \mathrm{SN} \\ 44 \mathrm{gpm} \end{gathered}$ | $\begin{aligned} & 14.2^{\prime} \\ & 9 \mathrm{SN} \end{aligned}$ $36 \mathrm{gpm}$ | $\begin{gathered} 14.9 \\ 9 \mathrm{SN} \\ 30 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 15.5^{\prime} \\ 9 \mathrm{SN} \\ 26 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 16.2^{\prime} \\ 10 \mathrm{SN} \\ 60 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 16.8^{\prime} \\ 10 \mathrm{SN} \\ 54 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 17.5^{\prime} \\ 10 \mathrm{SN} \\ 48 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 18.1^{\prime} \\ 10 \mathrm{SN} \\ 42 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 18.8^{\prime} \\ 10 \mathrm{SN} \\ 39 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 19.4^{\prime} \\ 10 \mathrm{SN} \\ 33 \mathrm{gpm} \end{gathered}$ |
| 10' | $\begin{gathered} 11.3^{\prime} \\ 9 \mathrm{SN} \\ 62 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 12.0^{\prime} \\ 9 \mathrm{SN} \\ 56 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 12.6^{\prime} \\ 9 \mathrm{SN} \\ 50 \mathrm{gpm} \\ \hline \end{gathered}$ | $\begin{gathered} 13.3^{\prime} \\ 9 \mathrm{SN} \\ 44 \mathrm{gpm} \end{gathered}$ | $13.9^{\prime}$ 9SN 39 gpm | $\begin{array}{r} 14.6^{\prime} \\ 9 \mathrm{SN} \\ 33 \mathrm{gpm} \\ \hline \end{array}$ | $\begin{gathered} 15.2^{\prime} \\ 9 \mathrm{SN} \\ 28 \mathrm{gpm} \end{gathered}$ | $15.9^{\prime}$ $10 \mathrm{SN}$ $62 \mathrm{gpm}$ | $\begin{gathered} 16.5^{\prime} \\ 10 \mathrm{SN} \\ 56 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 17.2^{\prime} \\ 10 \mathrm{SN} \\ 50 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 17.8^{\prime} \\ 10 \mathrm{SN} \\ 46 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 18.5^{\prime} \\ 10 \mathrm{SN} \\ 40 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 19.1^{\prime} \\ 10 \mathrm{SN} \\ 35 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 19.8^{\prime} \\ 10 \mathrm{SN} \\ 32 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 20.4^{\prime} \\ 10 \mathrm{SN} \\ 27 \mathrm{gpm} \end{gathered}$ |
| 11' | $\begin{gathered} 12.3^{\prime} \\ 9 \mathrm{SN} \\ 53 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 13.0^{\prime} \\ 9 \mathrm{SN} \\ 46 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 13.6^{\prime} \\ 9 \mathrm{SN} \\ 42 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 14.3^{\prime} \\ 9 \mathrm{SN} \\ 35 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 14.9^{\prime} \\ 9 \mathrm{SN} \\ 30 \mathrm{gpm} \\ \hline \end{gathered}$ | $\begin{array}{r} 15.6^{\prime} \\ 9 \mathrm{SN} \\ 25 \mathrm{gpm} \\ \hline \end{array}$ | $\begin{gathered} 16.2^{\prime} \\ 10 \mathrm{SN} \\ 60 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 16.9^{\prime} 1 \\ 10 \mathrm{SN} \\ 53 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 17.5^{\prime} \\ 10 \mathrm{SN} \\ 48 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 18.2^{\prime} \\ 10 \mathrm{SN} \\ 42 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 18.8^{\prime} \\ 10 \mathrm{SN} \\ 39 \mathrm{gpm} \\ \hline \end{gathered}$ | $\begin{gathered} 19.5^{\prime} \\ 10 \mathrm{SN} \\ 33 \mathrm{gpm} \\ \hline \end{gathered}$ | $\begin{gathered} 20.1 ' \\ 10 \mathrm{SN} \\ 29 \mathrm{gpm} \end{gathered}$ | $\begin{array}{r} 20.8^{\prime} \\ 10 \mathrm{SN} \\ 25 \mathrm{gpm} \\ \hline \end{array}$ | $\begin{gathered} 21.4^{\prime} \\ 14 \mathrm{~S} \\ 27 \mathrm{gpm} \end{gathered}$ |
| $12^{\prime}$ | $\begin{gathered} 13.3^{\prime} \\ 9 \mathrm{SN} \\ 44 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 14.0^{\prime} \\ 9 \mathrm{SN} \\ 40 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 14.6^{\prime} \\ 9 \mathrm{SN} \\ 33 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 15.3^{\prime} \\ 9 \mathrm{SN} \\ 27 \mathrm{gpm} \\ \hline \end{gathered}$ | $15.9^{\prime}$ <br> 10SN <br> 62 gpm | $\begin{gathered} 16.6^{\prime} \\ 10 \mathrm{SN} \\ 55 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 17.2^{\prime} \\ 10 \mathrm{SN} \\ 50 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 17.9 ' \\ 10 \mathrm{SN} \\ 45 \mathrm{gpm} \end{gathered}$ | $18.5^{\prime}$ 10SN <br> 40 gpm | $\begin{array}{r} 19.2^{\prime} \\ 10 \mathrm{SN} \\ 34 \mathrm{gpm} \\ \hline \end{array}$ | $\begin{array}{r} 19.8^{\prime} \\ 10 \mathrm{SN} \\ 32 \mathrm{gpm} \\ \hline \end{array}$ | $\begin{array}{r} 20.5^{\prime} \\ 10 \mathrm{SN} \\ 26 \mathrm{gpm} \\ \hline \end{array}$ | $\begin{gathered} 21.1^{\prime} \\ 14 \mathrm{~S} \\ 30 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 21.8^{\prime} \\ 14 \mathrm{~S} \\ 26 \mathrm{gpm} \end{gathered}$ | $\begin{array}{\|c\|} \hline 16.4^{\prime} \\ 16 \mathrm{~S} \\ 120 \mathrm{gpm}^{*} \end{array}$ |
| $13^{\prime}$ | $\begin{array}{r} 14.3^{\prime} \\ 9 \mathrm{SN} \\ 35 \mathrm{gpm} \\ \hline \end{array}$ | $\begin{array}{r} 15.0^{\prime} \\ 9 \mathrm{SN} \\ 29 \mathrm{gpm} \end{array}$ | $\begin{gathered} 15.6^{\prime} \\ 9 \mathrm{SN} \\ 25 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 16.3^{\prime} \\ 10 \mathrm{SN} \\ 58 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 16.9 \\ 10 \mathrm{SN} \\ 53 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 17.6^{\prime} \\ 10 \mathrm{SN} \\ 47 \mathrm{gpm} \\ \hline \end{gathered}$ | $\begin{array}{r} 18.2^{\prime} \\ 10 \mathrm{SN} \\ 42 \mathrm{gpm} \\ \hline \end{array}$ | $\begin{gathered} 18.9^{\prime} \\ 10 \mathrm{SN} \\ 37 \mathrm{gpm} \\ \hline \end{gathered}$ | $\begin{gathered} 19.5^{\prime} \\ 10 \mathrm{SN} \\ 33 \mathrm{gpm} \\ \hline \end{gathered}$ | $\begin{array}{r} 20.2^{\prime} \\ 10 \mathrm{SN} \\ 28 \mathrm{gpm} \\ \hline \end{array}$ | $\begin{gathered} 20.8^{\prime} \\ 10 \mathrm{SN} \\ 25 \mathrm{gpm} \\ \hline \end{gathered}$ | $\begin{gathered} 22.0^{\prime} \\ 14 \mathrm{~S} \\ 25 \mathrm{gpm} \end{gathered}$ | $\begin{array}{\|c\|} \hline 17.6^{\prime} \\ 16 \mathrm{~S} \\ 113 \mathrm{gpm} * \\ \hline \end{array}$ | $\begin{array}{\|c\|} \hline 17.9 \\ 16 \mathrm{~S} \\ 112 \mathrm{gpm} \star \\ \hline \end{array}$ | $\begin{array}{\|c\|} \hline 18.2^{\prime} \\ 16 \mathrm{~S} \\ 111 \mathrm{gpm} * \\ \hline \end{array}$ |
| $14^{\prime}$ | $\begin{gathered} 15.3^{\prime} \\ 9 S \mathrm{~N} \\ 27 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 16.0^{\prime} \\ 10 \mathrm{SN} \\ 61 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 16.6^{\prime} \\ 10 \mathrm{SN} \\ 55 \mathrm{gpm} \end{gathered}$ | $17.3^{\prime}$ 1OSN <br> 49 gpm | $17.9^{\prime}$ <br> 10SN 45 gpm | $\begin{gathered} 18.6^{\prime} \\ 14 \mathrm{~S} \\ 39 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 19.2^{\prime} \\ 10 \mathrm{SN} \\ 34 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 19.9^{\prime} \\ 10 \mathrm{SN} \\ 31 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 20.5^{\prime} \\ 10 \mathrm{SN} \\ 26 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 21.2^{\prime} \\ 14 \mathrm{~S} \\ 29 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 21.8^{\prime} \\ 14 \mathrm{~S} \\ 26 \mathrm{gpm} \end{gathered}$ | $\begin{array}{\|c\|} \hline 17.6^{\prime} \\ 16 \mathrm{~S} \\ 113 \mathrm{gpm} \end{array}$ | $\begin{array}{\|c\|} \hline 17.9^{\prime} \\ 16 \mathrm{~S} \\ 112 \mathrm{gpm} \end{array}$ | $\begin{array}{\|c\|} \hline 18.2^{\prime} \\ 16 \mathrm{~S} \\ 111 \mathrm{gpm} * \end{array}$ | $\begin{gathered} 18.4^{\prime} \\ 16 \mathrm{~S} \\ 110 \mathrm{gpm}^{\star} \end{gathered}$ |
| 15' | $\begin{gathered} 16.3^{\prime} \\ 10 \mathrm{SN} \\ 58 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 17.0^{\prime} \\ 10 \mathrm{SN} \\ 52 \mathrm{gpm} \\ \hline \end{gathered}$ | 17.6' 10SN 47 gpm | 18.3' 10SN 41 gpm | 18.9' 10SN 37 gpm | $\begin{gathered} 19.6^{\prime} \\ 10 \mathrm{SN} \\ 33 \mathrm{gpm} \\ \hline \end{gathered}$ | $\begin{gathered} 20.2^{\prime} \\ 10 \mathrm{SN} \\ 28 \mathrm{gpm} \\ \hline \end{gathered}$ | $\begin{array}{r} 20.9 \\ 10 \mathrm{SN} \\ 25 \mathrm{gpm} \\ \hline \end{array}$ | $\begin{gathered} 21.5^{\prime} \\ 14 \mathrm{~S} \\ 27 \mathrm{gpm} \\ \hline \end{gathered}$ | $\begin{gathered} 22.2^{\prime} \\ 14 \mathrm{~S} \\ 25 \mathrm{gpm} \\ \hline \end{gathered}$ | $\begin{array}{\|c\|} \hline 18.3^{\prime} \\ 16 \mathrm{~S} \\ 110 \mathrm{gpm} \end{array}$ | $\begin{array}{\|c\|} \hline 18.6^{\prime} \\ 16 \mathrm{~S} \\ 109 \mathrm{gpm} * \\ \hline \end{array}$ | $\begin{array}{\|c\|} \hline 18.9 \\ 16 \mathrm{~S} \\ 107 \mathrm{gpm} \end{array}$ | $\begin{array}{\|c\|} 19.2^{\prime} \\ 16 \mathrm{~S} \\ 105 \mathrm{gpm} \end{array}$ | $\begin{array}{\|c\|} \hline 19.4 \\ 16 \mathrm{~S} \\ 104 \mathrm{gpm} \end{array}$ |
| $16^{\prime}$ | $17.3^{\prime}$ $10 \mathrm{SN}$ $49 \mathrm{gpm}$ | $\begin{gathered} 18.0^{\prime} \\ 10 \mathrm{SN} \\ 44 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 18.6^{\prime} \\ 10 \mathrm{SN} \\ 39 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 19.3^{\prime} \\ 10 \mathrm{SN} \\ 33 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 19.9 \\ 10 \mathrm{SN} \\ 31 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 20.6^{\prime} \\ 10 \mathrm{SN} \\ 25 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 21.2^{\prime} \\ 14 \mathrm{~S} \\ 29 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 21.9^{\prime} \\ 14 \mathrm{~S} \\ 26 \mathrm{gpm} \end{gathered}$ | $\begin{array}{\|c\|} \hline 18.8 \\ 16 \mathrm{~S} \\ 107 \mathrm{gpm} * \end{array}$ | $\begin{array}{\|c\|} \hline 19.1^{\prime} \\ 16 \mathrm{~S} \\ 105 \mathrm{gpm} * \end{array}$ | $\begin{array}{\|c\|} \hline 19.3 ' \\ 16 \mathrm{~S} \\ 104 \mathrm{gpm} * \end{array}$ | $\begin{array}{\|c\|} \hline 19.6^{\prime} \\ 16 \mathrm{~S} \\ 103 \mathrm{gpm} \end{array}$ | $\begin{array}{\|c\|} \hline 19.9 ' \\ 16 \mathrm{~S} \\ 101 \mathrm{gpm}^{\star} \end{array}$ | $\begin{gathered} 20.2^{\prime} \\ 16 \mathrm{~S} \\ 98 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 21.2^{\prime} \\ 16 \mathrm{~S} \\ 95 \mathrm{gpm} \end{gathered}$ |
| 17' | $18.3^{\prime}$ $10 \mathrm{SN}$ <br> 41 gpm | $\begin{gathered} 19.0^{\prime} \\ 10 \mathrm{SN} \\ 36 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 19.6^{\prime} \\ 10 \mathrm{SN} \\ 33 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 20.3^{\prime} \\ 10 \mathrm{SN} \\ 27 \mathrm{gpm} \end{gathered}$ | 20.9' <br> 10SN 25 gpm | $\begin{gathered} 21.6^{\prime} \\ 14 \mathrm{~S} \\ 26 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 22.2^{\prime} \\ 14 \mathrm{~S} \\ 25 \mathrm{gpm} \end{gathered}$ | $\begin{array}{\|c\|} \hline 19.5^{\prime} \\ 16 \mathrm{~S} \\ 103 \mathrm{gpm} \star \end{array}$ | $\begin{array}{\|c\|} \hline 19.8 ' \\ 16 \mathrm{~S} \\ 102 \mathrm{gpm} \end{array}$ | $\begin{array}{\|c\|} \hline 20.0 \\ 16 \mathrm{~S} \\ 100 \mathrm{gpm} \star \end{array}$ | $\begin{gathered} 20.3^{\prime} \\ 16 \mathrm{~S} \\ 99 \mathrm{gpm}{ }^{\star} \end{gathered}$ | $\begin{gathered} 20.6^{\prime} \\ 16 \mathrm{~S} \\ 98 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 20.9 \\ 16 \mathrm{~S} \end{gathered}$ <br> 97 gpm* | $\begin{gathered} 21.2^{\prime} \\ 16 \mathrm{~S} \\ 95 \mathrm{gpm} * \end{gathered}$ | $\begin{gathered} 22.4^{\prime} \\ 16 \mathrm{~S} \\ 95 \mathrm{gpm} \end{gathered}$ |
| 18' | $\begin{gathered} 19.3^{\prime} \\ 10 \mathrm{SN} \\ 33 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 20.0^{\prime} \\ 10 \mathrm{SN} \\ 30 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 20.6^{\prime} \\ 10 \mathrm{SN} \\ 25 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 21.3^{\prime} \\ 14 \mathrm{~S} \\ 28 \mathrm{gpm} \end{gathered}$ | $21.9$ $14 \mathrm{~S}$ <br> 26 gpm | $\begin{gathered} 19.9 \\ 16 \mathrm{~S} \\ 101 \mathrm{gpm}^{\star} \end{gathered}$ | $\begin{gathered} 20.2^{\prime} \\ 16 \mathrm{~S} \\ 98 \mathrm{gpm} \end{gathered}$ | $\begin{array}{\|c\|} \hline 20.5^{\prime} \\ 16 \mathrm{~S} \\ 98 \mathrm{gpm} \end{array}$ | $\begin{gathered} 20.8^{\prime} \\ 16 \mathrm{~S} \\ 97 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 21.1 \mathrm{l} \\ 16 \mathrm{~S} \\ 96 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 21.3^{\prime} \\ 16 \mathrm{~S} \\ 95 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 22.6^{\prime} \\ 16 \mathrm{~S} \\ 93 \mathrm{gpm} * \end{gathered}$ | $\begin{gathered} 21.9 \\ 16 \mathrm{~S} \\ 91 \mathrm{gpm} \end{gathered}$ | 22.2 <br> 16S 90 gpm* | 22.4' <br> 16S <br> 89 gpm* |
| $19 '$ | $\begin{gathered} 20.3^{\prime} \\ 10 \mathrm{SN} \\ 27 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 21.0^{\prime} \\ 14 \mathrm{~S} \\ 30 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 21.6^{\prime} \\ 14 \mathrm{~S} \\ 26 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 22.3^{\prime} \\ 14 \mathrm{~S} \\ 25 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 20.7^{\prime} \\ 16 \mathrm{~S} \\ 98 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 21.0^{\prime} \\ 16 \mathrm{~S} \\ 96 \mathrm{gpm}^{*} \end{gathered}$ | $\begin{gathered} 21.2^{\prime} \\ 16 \mathrm{~S} \\ 95 \mathrm{gpm} * \end{gathered}$ | $\begin{array}{\|c\|} \hline 22.5^{\prime} \\ 16 \mathrm{~S} \\ 94 \mathrm{gpm} \end{array}$ | $\begin{gathered} \hline 21.8^{\prime} \\ 16 \mathrm{~S} \\ 92 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 22.1^{\prime} \\ 16 \mathrm{~S} \\ 91 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 22.3^{\prime} \\ 16 \mathrm{~S} \\ 90 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 22.6^{\prime} \\ 16 S \end{gathered}$ <br> 86 gpm* | $\begin{gathered} 22.9^{\prime} \\ 16 \mathrm{~S} \\ 84 \mathrm{gpm}^{*} \end{gathered}$ | $\begin{gathered} 23.2^{\prime} \\ 16 \mathrm{~S} \\ 82 \mathrm{gpm} * \end{gathered}$ | $\begin{gathered} 23.4^{\prime} \\ 16 \mathrm{~S} \end{gathered}$ <br> 81 gpm* |
| $20^{\prime}$ | $\begin{gathered} 21.3^{\prime} \\ 14 \mathrm{~S} \\ 28 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 22.0^{\prime} \\ 14 \mathrm{~S} \\ 25 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 21.6^{\prime} \\ 16 \mathrm{~S} \\ 95 \mathrm{gpm}^{\star} \end{gathered}$ | $\begin{gathered} 21.9 \\ 16 \mathrm{~S} \\ 95 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 22.2^{\prime} \\ 16 \mathrm{~S} \\ 95 \mathrm{gpm}^{\star} \end{gathered}$ | $\begin{gathered} 22.5^{\prime} \\ 16 \mathrm{~S} \\ 88 \mathrm{gpm}^{*} \end{gathered}$ | $\begin{gathered} 22.8^{\prime} \\ 16 \mathrm{~S} \\ 85 \mathrm{gpm} * \end{gathered}$ | $\begin{gathered} 23.1^{\prime} \\ 16 \mathrm{~S} \\ 83 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 23.4^{\prime} \\ 16 \mathrm{~S} \\ 81 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 23.7^{\prime} \\ 16 \mathrm{~S} \\ 80 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 24.0^{\prime} \\ 16 \mathrm{~S} \\ 79 \mathrm{gpm} \end{gathered}$ | $\begin{gathered} 24.3^{\prime} \\ 16 \mathrm{~S} \\ 78 \mathrm{gpm} \end{gathered}$ | $24.6^{\prime}$ $16 \mathrm{~S}$ <br> 77 gpm* | $\begin{gathered} 24.9^{\prime} \\ 16 \mathrm{~S} \\ 76 \mathrm{gpm} * \end{gathered}$ | $\begin{gathered} 25.2^{\prime} \\ 16 \mathrm{~S} \end{gathered}$ <br> 75 gpm* |

## Guidelines for Sizing

Figure 7.
Flow - Liters/Minute


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